

Fig. 2 Jet centerlines.

is any function of m . Equation (8) is seen to be of this form.

Figure 2 shows calculated jet centerlines using Eq. (7). Shown in the same figure are data from Ref. 7, and it is seen that Eq. (7) fits these experimental data quite well. Analysis of other experimental data^{8,9} has shown the same functional relationship, although for each set of test data better correlation can be obtained by using slightly different values for the coefficient and exponent of Eq. (7).

References

- Monical, R. E., "A Method of Representing Fan-Wing Combinations for Three-Dimensional Potential Flow Solutions," *Journal of Aircraft*, Vol. 2, No. 6, Nov.-Dec. 1965, pp. 527-530.
- Wooler, P. T., "On the Flow Past a Circular Jet Exhausting at Right Angles from a Flat Plate or Wing," *Journal of the Royal Aeronautical Society*, Vol. 71, March 1967, pp. 216-218.
- Rubbert, P. E. and Saaris, G. R., "A General Three-Dimensional Potential-Flow Method Applied to V/STOL Aerodynamics," Paper 680304, Society of Automotive Engineers.
- Wooler, P. T., Burghart, G. H., and Gallagher, J. T., "Pressure Distribution on a Rectangular Wing with a Jet Exhausting Normally into an Airstream," *Journal of Aircraft*, Vol. 4, No. 6, Nov.-Dec. 1967, pp. 537-543.
- Williams, J. and Wood, M. N., "Aerodynamic Interference Effects with Jet-Lift V/STOL Aircraft under Static and Forward Speed Conditions," *Zeitschrift für Flugwissenschaften*, Vol. 15, July 1967, pp. 238-256.
- Wooler, P. T., "Calculation of the Forces on a Wing Due to a Circular Jet Exhausting from the Lower Surface of a Wing into a Uniform Airstream," PhD thesis, May 1964, University of Manchester, England.
- Jordinson, R., "Flow in a Jet Directed Normal to the Wind," R & M 3074 1958, British Aeronautical Research Council.
- Keffer, J. F. and Baines, W. D., "The Round Turbulent Jet in a Cross-Wind," *Journal of Fluid Mechanics*, Vol. 15, pt. 4, 1963, pp. 481-496.
- Gelb, G. H. and Martin, W. A., "An Experimental Investigation of the Flow Field about a Subsonic Jet Exhausting into a Quiescent and a Low Velocity Airstream," *Canadian Aeronautics and Space Journal*, Vol. 12, No. 8, Oct. 1966, pp. 333-342.

Skin-Friction Formula for Tapered and Delta Wings

ARNE BARKHEM*

SAAB Aktiebolag, Linköping, Sweden

WHEN determining the skin-friction drag for a tapered or delta-shaped wing, it is necessary to take into consideration the variation of the skin-friction coefficient over the whole surface and the dependence on the Reynolds' number spanwise variation with chord length. In principle this can be done in two ways. One method is to choose some equivalent reference chord on the wing for the calculation of the skin-friction coefficient. This method can however give considerable errors. The other method of analysis is to integrate the skin-friction coefficient along the span of the wing, the so-called strip integration method. If the skin-friction formula used is simple enough for the integral to be developed into an explicit expression, the analysis is quite straightforward. Unfortunately, this is not always the case. For the skin friction in turbulent boundary layer, the formulas commonly used will require numerical integration. This can be very time consuming. Much time could be saved if there existed a formula which made the numerical integration unnecessary. The following is such a formula for a tapered surface (one side of the wing) with fully turbulent boundary layer:

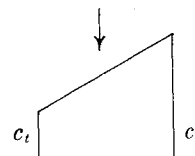
$$c_f = \frac{0.472}{\left({}^{10}\log Re \frac{1 + \lambda}{2} \right)^{2.58}} \left[1 - \frac{(1 - \lambda)^4 (4.55 - 0.27 \cdot {}^{10}\log Re)}{100} \right]$$

where Re = Reynolds number based on c_r ($c_r > c_t$)

$$\lambda = \frac{c_t}{c_r}$$

c_r = root chord

c_t = tip chord



The formula has been developed by correlating the λ and Re dependence against values calculated by complete integration, using the Prandtl flat-plate turbulent skin-friction formula

$$c_f = 0.472 / ({}^{10}\log Re)^{2.58}$$

For the Reynolds number range $10^5 - 10^9$, the formula agrees within 0.2% with strip-integrated values.

Received November 26, 1968; revision received January 20, 1969.

* Aerodynamicist.